

Short communication

## NO<sub>x</sub> uptake capacities and sequestration pathways by hydrated cementitious phases

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## ABSTRACT

This study seeks to quantify NO<sub>x</sub> sequestration by individual hydrated cementitious phases (C-S-H, AFm-SO<sub>4</sub>, and Ca(OH)<sub>2</sub>), establish a fundamental understanding of the reaction pathways, and reveal the effects of carbonation (CaCO<sub>3</sub> and AFm-CO<sub>3</sub>). For uncarbonated phases, the highest NO<sub>x</sub> uptake was measured in C-S-H, with the produced nitrite/nitrate physically bound on solid surface. For AFm-SO<sub>4</sub>, an anion exchange process was observed, where nitrite/nitrate substitute for sulfate and form new AFm-NO<sub>2</sub>/NO<sub>3</sub>. Ca(OH)<sub>2</sub> showed undetectable NO<sub>x</sub> uptake, which may be due to the relative low temperature and relative humidity. For carbonated phases, CaCO<sub>3</sub> exhibited an improved NO<sub>x</sub> uptake compared to uncarbonated phases, with uptake capacity three times higher than that of C-S-H. The result of AFm-CO<sub>3</sub> indicates that carbonation could potentially inhibit the anion exchange process that was observed in AFm-SO<sub>4</sub>. These findings provide guidelines for the rational design and optimization of cement-based materials for enhanced NO<sub>x</sub> sequestration.

### 1. Introduction

Nitrogen oxides (NO<sub>x</sub>) are one of the primary causes of the formation of tropospheric ozone and urban smog [1]. Together with sulfur oxides (SO<sub>x</sub>), NO<sub>x</sub> contribute to acid rain, which damages the natural and built environment. Additionally, NO<sub>x</sub> impair the human respiratory and visual systems causing a variety of health problems [1]. To address atmospheric NO<sub>x</sub> levels, researchers have proposed using nano photocatalytic TiO<sub>2</sub> in cement-based materials [2–4]. The NO<sub>x</sub> uptake capacities for both TiO<sub>2</sub>-modified and ordinary cementitious materials demonstrate that properly designed cement-based materials can serve as a potential NO<sub>x</sub> sink [5,6].

NO<sub>x</sub> sequestration in conventional and TiO<sub>2</sub>-modified cement-based materials has been theorized as a two-step process: (1) the conversion of NO<sub>x</sub> to nitrite (NO<sub>2</sub><sup>-</sup>) and/or nitrate (NO<sub>3</sub><sup>-</sup>), and (2) the binding of NO<sub>2</sub><sup>-</sup>/NO<sub>3</sub><sup>-</sup> within the hydrated cementitious phases. The NO<sub>x</sub> conversion mechanisms (Step 1) can be summarized in three primary mechanisms:

- i. In the presence of TiO<sub>2</sub> photocatalysts, the photocatalytic reactions upon exposure to NO<sub>x</sub> and UV light convert NO<sub>x</sub> into NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> [2,7,8];

- ii. In the absence of TiO<sub>2</sub> photocatalysts, surface catalyzed heterogeneous reactions, which are intrinsic to cementitious materials, promote the conversion of NO<sub>x</sub> to NO<sub>2</sub><sup>-</sup> and/or NO<sub>3</sub><sup>-</sup> [4,9]. Higher surface area is expected to enhance the reaction [10]. These reactions can also be facilitated by the monolayers of water on the surfaces and within the pore solution in the cementitious materials [4,9] (see below);
- iii. The alkalinity intrinsic to cementitious materials also aids in the transformation of NO<sub>x</sub> to NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> through the reactions between NO<sub>x</sub> and hydroxyls present in the pore solution [11,12].

In contrast, the binding mechanism(s) (Step 2) are less understood, with only a few studies attempting to elucidate the mechanism(s) [13,14]. For example, Kaja et al. [15] indicated that the presence of capillary pores in cement-based materials with sizes of 10–50 nm could help increase NO<sub>x</sub> binding efficiency. Their work also demonstrated that the carbonation of these materials could increase the formation of capillary pores and in turn enhance photocatalytic efficiency for NO<sub>x</sub> conversion [15].

To understand the essential pathways for NO<sub>x</sub> binding in cementitious materials, direct examinations of the binding mechanisms are

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desired, especially for NO<sub>x</sub> interactions with individual cementitious phases. The hydrated and carbonated phases present in concrete vary in structure and composition, and each can have different impacts on the mechanism(s), efficiency, and permanency for NO<sub>x</sub> binding. It is unclear whether NO<sub>x</sub> is bound within the cementitious material as one or multiple N-containing species, or whether it is sequestered within the cementitious matrix as adsorbed species on the surface of cementitious hydrates, substituted into ordered structures, or dissolved in pore solution. The relative permanency of the NO<sub>x</sub> binding mechanism is also important to understand [5]. For instance, our previous studies [5,6] demonstrated that different cements (e.g., portland cement versus calcium aluminate cement) with different chemical composition and hydration products could result in different binding mechanisms, which can lead to over- or under-estimation of the material's NO<sub>x</sub> uptake capacity. Therefore, such mechanistic information is critical for designing cement-based materials with desired properties and chemical compositions for enhanced NO<sub>x</sub> sequestration.

To address the above discussed knowledge gaps, this study investigates the interaction of NO<sub>x</sub> with individual cement hydration products in order to understand the roles of different phases in the mechanisms and capacity for NO<sub>x</sub> uptake. Three main hydrated phases in portland cement-based materials are synthesized and exposed to NO<sub>x</sub> directly, including calcium silicate hydrate (C-S-H), portlandite (Ca(OH)<sub>2</sub>), and mono-sulfoaluminate (AFm-SO<sub>4</sub>). To investigate the effects of carbonation, calcite (CaCO<sub>3</sub>) and mono-carboaluminate (AFm-CO<sub>3</sub>) were selected since these are the most stable carbonated phases in concrete [16]. In cement-based materials during environmental exposure, these two phases result from the natural carbonation of Ca(OH)<sub>2</sub> and C-S-H, and AFm phases, respectively. To quantify the NO<sub>x</sub> sequestration capacity and evaluate the binding mechanism for each cementitious phase, a combination of wet chemical extraction, ultraviolet-visible spectrophotometry, and ion chromatography is employed. In addition, X-ray diffraction (XRD) is used to identify changes in mineralogy upon NO<sub>x</sub> exposure. Understanding the intrinsic NO<sub>x</sub> binding capacity of individual cement phases can facilitate the estimation of concrete's potential for NO<sub>x</sub> sequestration and the optimization of composition for this function.

## 2. Material and methods

### 2.1. Materials

C-S-H was synthesized from triclinic alite (C<sub>3</sub>S) and silica fume. C<sub>3</sub>S was obtained from Mineral Research Processing (Meyzieu, France) and its purity was determined by quantitative XRD using the Rietveld method to be 95 ± 1.5 %. The silica fume (42,741 Silicon (IV) oxide, amorphous fumed) was obtained from Alfa Aesar (Ward Hill, MA, USA) with stated purity exceeding 95 % and surface area of 300–350 m<sup>2</sup> g<sup>-1</sup>. Based on well-established stoichiometry of C-S-H [17] and synthesizing methods [18], 5 g of alite and 1.53 g of silica fume were selected to synthesize C-S-H with a C/S ratio of approximately 1.7 with the sample preparation detailed below. Silica fume was first suspended in 250 g of N<sub>2</sub>-degassed deionized water (18.2 MΩ·cm) and stirred for three minutes. Alite was then added to the silica suspension and stirred at 23 ± 2 °C for a week, during which the entire setup was sealed by Parafilm to avoid carbonation. The liquid-to-solid ratio is about 50 by weight to ensure complete reaction and to prevent the formation of calcium hydroxide. At the end of reaction, the suspension was filtered using Whatman grade 1 filter paper and the obtained solids were vacuum dried at 23 ± 2 °C and stored in a doubly sealed inert high-density polyethylene (HDPE) bottle prior to NO<sub>x</sub> exposure and characterization.

AFm-SO<sub>4</sub> and AFm-CO<sub>3</sub> were synthesized according to the protocol developed by Matschei [19]. AFm-SO<sub>4</sub> was prepared by mixing C<sub>3</sub>A (preparation procedure in the next paragraph) and CaSO<sub>4</sub> in a 1:1 M ratio in boiling deionized water with water/solid mass ratio of around 20. The slurry was then stirred at 85 °C for two weeks in a sealed

polytetrafluoroethylene (PTFE) bottle prior to filtration with Whatman grade 1 filter paper and vacuum-drying. AFm-CO<sub>3</sub> was prepared by mixing C<sub>3</sub>A and CaCO<sub>3</sub> in a 1:1 M ratio at 23 ± 2 °C with a water/solid mass ratio of around 20. The mixture was stirred in PTFE-bottles for two weeks prior to filtration and vacuum-drying.

C<sub>3</sub>A was prepared by combining analytical reagent grade CaCO<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub> (certified purity of ≥99 %) in a 3:1 M ratio. The powders were dry-mixed, homogenized, and pressed into pellets at a pressure of 10 MPa. The pellets were placed in zirconia grain-hardened platinum crucibles and sintered at 1450 °C in a muffle furnace for a 24-h period. At the end of the sintering routine, the pellets were air quenched. The pelletized, sintered material was finely ground and pelletized once again, and the sintering routine repeated two more times. After preparation, the C<sub>3</sub>A was stored in a doubly sealed HDPE bottle at 23 ± 2 °C until use.

Ca(OH)<sub>2</sub> was reagent grade (Acros, Thermo Fisher Scientific Pittsburgh, PA, USA) with a stated purity exceeding 98 %. CaCO<sub>3</sub> was also reagent grade (Alfa Aesar, Ward Hill, MA, USA) with a certified purity of ≥99 %.

### 2.2. NO<sub>x</sub> exposure

Fig. 1 illustrates the NO<sub>x</sub> exposure test 'plug-flow' setup based on ISO 22197 [20] and JIS R 1701 Standards [21]. For the test, 1.00 ± 0.01 g of a powdered phase was placed in weighing boats, which resided at the bottom of a borosilicate reactor with both ends sealed with a filter and screw cap. Each phase was tested separately. The NO<sub>x</sub> gas is prepared based on the aforementioned standards and comprises 1000 ppb nitric oxide (NO) gas with ultrapure dry air. The gas passed through the photoreactor at a constant flow rate of 1 L min<sup>-1</sup>. For Ca(OH)<sub>2</sub>, the NO<sub>x</sub> gas contains 1000 ppb nitric oxide gas with N<sub>2</sub> gas to prevent any potential carbonation during the exposure test. The reaction was conducted at 23 ± 2 °C and 50 ± 2 % relative humidity by passing the gas through a humidifier. The samples were continuously exposed to NO<sub>x</sub> gas for 5 h to ensure an ultimate NO<sub>x</sub> binding capacity has been reached. The inlet gas concentration stayed at 1000 ppb, which was measured by a chemiluminescent NO/NO<sub>2</sub>/NO<sub>x</sub> analyzer (Model 200A, Teledyne API). Since this study focuses on examining the interaction between NO<sub>x</sub> and hydrated cementitious phases, we omit the inclusion of photocatalytic TiO<sub>2</sub> particles and the UV light exposure compared to the previous studies [5,6]. The entire test setup was covered by a black light-blocking canvas to prevent potential interference from ambient light. After NO<sub>x</sub> exposure, samples were stored in double sealed plastic bags prior to nitrite/nitrate detection tests. Control samples without NO<sub>x</sub> exposure were also tested.

### 2.3. NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> detection

The experimental method for detecting NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> combines wet extraction, UV-vis spectrophotometry, and ion chromatography. The wet chemical extraction was performed by suspending 0.1 g of NO<sub>x</sub>-exposed powders in 40 mL anoxic deionized water (18.2 MΩ·cm, purged with N<sub>2</sub> gas for 48 h) in HDPE bottles. The HDPE bottles were wrapped in aluminum foil to prevent ambient light from affecting the reaction. All bottles were placed on a shaker at 150 rpm for 48 h. After the extraction, the suspension was filtered through a 0.45 μm syringe filter and the filtrate was then analyzed for both nitrite and nitrate concentrations. Three replicates for the wet extraction of each NO<sub>x</sub>-solid reaction were prepared for each phase for the nitrite and nitrate detection.

Nitrite concentration was determined using a colorimetric assay kit (Roche, Sigma Aldrich, St. Louis, MO, USA) and measured at 540 nm on a UV-vis spectrometer (Cary 60, Agilent, Santa Clara, CA, USA). Nitrate concentration was determined using an ion chromatography unit (Dionex, Sunnyvale, CA) equipped with an Ionpac® AS14A column (4 × 250 mm) combined with an Ionpac® AG14A guard column (4 × 50 mm) and a Dionex ED40 electrochemical detector. The mobile phase used for ion chromatography contained a mixture of 8 mM Na<sub>2</sub>CO<sub>3</sub> and 1 mM

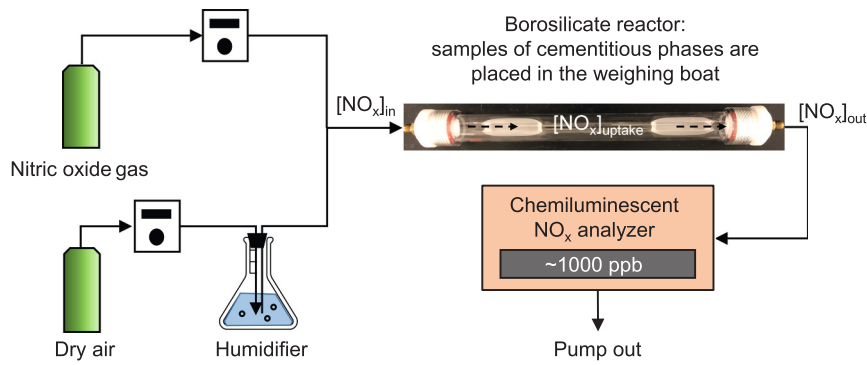


Fig. 1. Experimental setup for NO<sub>x</sub> exposure.

NaHCO<sub>3</sub>, and the flow rate was 0.8 mL min<sup>-1</sup>.

The total nitrogen (N) mass of NO<sub>x</sub> uptake, which was used to represent the measured nitrite and nitrate masses, was determined using Eqs. (1)–(4). For the purpose of comparison, the specific NO<sub>x</sub> uptake is normalized by sample mass (this method has been previously demonstrated and validated in refs [5,6]) and with a unit of mg N per kg solid and is denoted as mg kg<sup>-1</sup> for simplicity.

$$m_{NO_2^-} = C_{NO_2^-} \times DF \quad (1)$$

$$m_{NO_3^-} = C_{NO_3^-} \times DF \quad (2)$$

$$m'_N = m_{NO_2^-} \times \frac{M_N}{M_{NO_2^-}} \quad (3)$$

$$m'_N = m_{NO_3^-} \times \frac{M_N}{M_{NO_3^-}} \quad (4)$$

where  $M_{NO_2^-}$  = the mass of nitrite (mg kg<sup>-1</sup>),  $M_{NO_3^-}$  = the mass of nitrate (mg kg<sup>-1</sup>),  $C_{NO_2^-}$  = the concentration of nitrite measured by UV–vis spectrometer (ppm),  $C_{NO_3^-}$  = the concentration of nitrate measured by ion chromatography (ppm), DF = dilution factor used for wet chemical extraction (400),  $m'_N$  = the mass of nitrogen from nitrite (mg kg<sup>-1</sup>),  $m'_N$  = the mass of nitrogen from nitrate (mg kg<sup>-1</sup>),  $M_{NO_2^-}$  = the molar mass of nitrite = 46 g mol<sup>-1</sup>, and  $M_{NO_3^-}$  = the molar mass of nitrate = 62 g mol<sup>-1</sup>.

#### 2.4. X-ray diffraction

XRD was performed on the synthetic cementitious phases before and after NO<sub>x</sub> exposure to identify changes in mineralogy. Approximately 0.2 g of powders were packed into a sample holder, and the measurements were taken on a PANalytical Empyrean X-ray diffractometer (Malvern Panalytical Ltd., Malvern, United Kingdom) with Cu Kα (λ = 1.54 Å) radiation at 45 kV and 40 mA. Scans were performed at 5–45° 2θ using a PIXcel3D detector and analyzed with PANalytical HighScore Plus software.

### 3. Results

To understand the pathways for NO<sub>x</sub> sequestration, quantify NO<sub>x</sub> uptake capacity by each cementitious phase, and understand the effect of carbonation on NO<sub>x</sub> uptake, five synthetic cementitious phases that are common in cementitious materials were synthesized and subjected to NO<sub>x</sub> exposure under the same conditions. The phases include calcium silicate hydrate (C-S-H), portlandite (Ca(OH)<sub>2</sub>), mono-sulfoaluminate (AFm-SO<sub>4</sub>), calcite (CaCO<sub>3</sub>), and mono-carboaluminate (AFm-CO<sub>3</sub>). NO<sub>x</sub> uptake capacity was measured by a combination of wet chemical extraction, UV–vis spectrophotometry, and ion chromatography.

The NO<sub>x</sub> conversion results of the measured N mass, combined from NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> detection, are shown in Fig. 2. Control samples without

NO<sub>x</sub> exposure showed no detectable NO<sub>2</sub><sup>-</sup> or NO<sub>3</sub><sup>-</sup>. Based on the combined results from NO<sub>2</sub><sup>-</sup>/NO<sub>3</sub><sup>-</sup> production and XRD analysis, the binding mechanism and NO<sub>x</sub> sequestration pathways for each cementitious phase are considered below.

#### 3.1. Calcium silicate hydrate (C-S-H)

Among three uncarbonated cementitious phases (C-S-H, Ca(OH)<sub>2</sub>, and AFm-SO<sub>4</sub>), C-S-H shows the highest NO<sub>x</sub> uptake capacity (calculated as the total amount of nitrite- and nitrate-N produced, Section 2.3), with nitrite measured at approximately 50 mg kg<sup>-1</sup> and nitrate at 150 mg kg<sup>-1</sup> (Fig. 2). The presence of higher nitrate concentration compared to nitrite concentration agrees with prior measurements on cement pastes [9]. A relatively high level of NO<sub>x</sub> uptake by C-S-H was expected because of the high surface area and the interlayer water molecules that promote heterogeneous catalytic reactions [17,22]. These relate to mechanism (ii), as described in the introduction. Additionally, gel pores are intrinsic to the C-S-H structure and typically contains alkaline pore solution [17,22], which suggests the potential for the formation of NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> ions [11] via mechanism (iii). Therefore, this study supports the hypothesis of our previous studies [5,10] that C-S-H, with its unique microstructural features, is favorable to NO<sub>x</sub> conversion and plays a major role in sequestering NO<sub>x</sub> in OPC-based cementitious materials. However, the capacity of C-S-H to bind NO<sub>x</sub> has not been previously quantified.

XRD analysis did not observe the formation of new peaks in samples with NO<sub>x</sub> exposure (Fig. 3). Given the amount of NO<sub>x</sub> sequestered by this phase, this indicates that the formation of new solid phases between C-S-

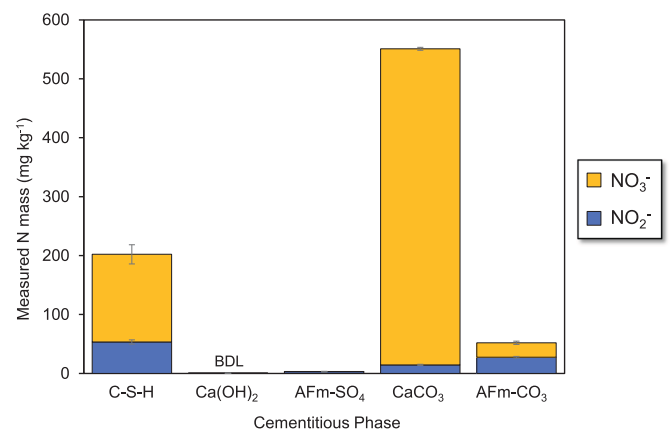
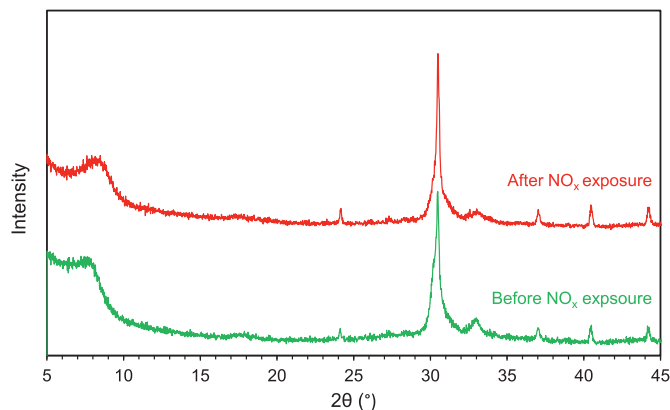


Fig. 2. Measured N mass as nitrite (NO<sub>2</sub><sup>-</sup>, blue) or nitrate (NO<sub>3</sub><sup>-</sup>, yellow) normalized by sample mass after the reaction of five synthetic cementitious phases with NO<sub>x</sub>. The phases include calcium silicate hydrate (C-S-H), portlandite (Ca(OH)<sub>2</sub>), mono-sulfoaluminate (AFm-SO<sub>4</sub>), calcite (CaCO<sub>3</sub>), and mono-carboaluminate (AFm-CO<sub>3</sub>). BDL: below detection limit.

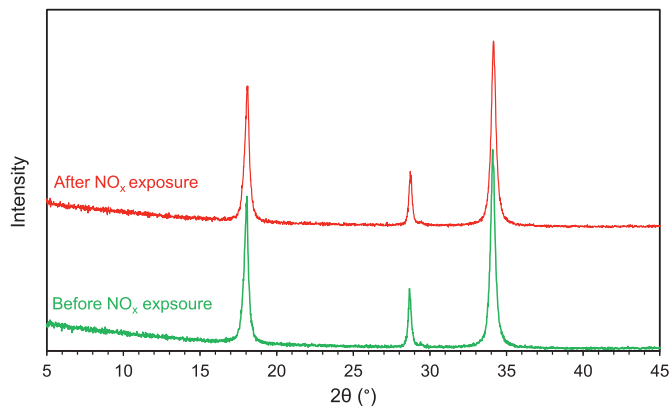
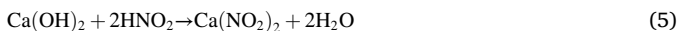


**Fig. 3.** XRD patterns of C-S-H phases before (control) and after NO<sub>x</sub> exposure indicating that the formation of new solid phases between C-S-H and NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> ions is unlikely because no new peaks or humps (indicative of new crystalline or amorphous phases, respectively) are detected.

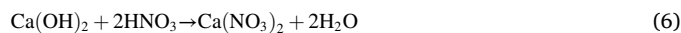
H and NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> ions is unlikely or only at minor amount below the detection limit (the detection limit of XRD for crystalline phase is typically around 5 %). The results also support the previously proposed hypothesis that NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> likely adsorb on the surface of C-S-H [10,15,23] or dissolve in the pore solution [10]. Either way, these ions are susceptible to wet chemical extraction and can be quantified by UV-vis spectrophotometry and ion chromatography. However, future studies are necessary to discern the relative significance of these two factors in NO<sub>x</sub> binding of C-S-H. For synthetic C-S-H, its surface area and morphology are not significantly affected by the Ca/Si ratio but governed by the lime concentration of C-S-H suspension [24,25]. Therefore, the effect of lime concentration should also be considered in the future study for the NO<sub>x</sub> uptake in C-S-H.

### 3.2. Portlandite (Ca(OH)<sub>2</sub>)

Ca(OH)<sub>2</sub> showed no detectable NO<sub>x</sub> uptake (Fig. 2), and no new phases were detected by XRD after NO<sub>x</sub> exposure (Fig. 4). These results indicate that Ca(OH)<sub>2</sub> could be intrinsically resistant to NO<sub>x</sub> sequestration, at least under the current experimental conditions. Interestingly, Zhang et al. [26] demonstrated atmospheric NO<sub>x</sub> removal by Ca(OH)<sub>2</sub>. They suggested the following reactions for the interaction of Ca(OH)<sub>2</sub> with produced nitrate and nitrite to form calcium nitrite and nitrate:



**Fig. 4.** The XRD patterns of Ca(OH)<sub>2</sub> phases before (control) and after NO<sub>x</sub> exposure indicates that Ca(OH)<sub>2</sub> under the current temperature and relative humidity conditions in this study could be resistant to NO<sub>x</sub> uptake because no new peaks (indicative of new crystalline) are detected.



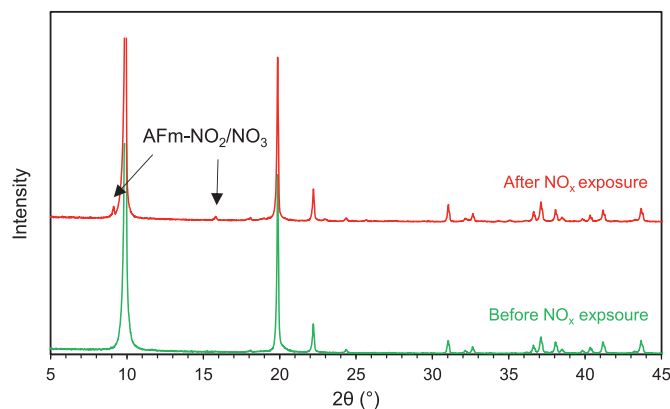
Because Ca(NO<sub>2</sub>)<sub>2</sub> and Ca(NO<sub>3</sub>)<sub>2</sub> are highly soluble, the resulting NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> ions should be detectable through wet chemical extraction such as that used in our study. However, their experiments were performed at 70 °C and a relative humidity of 60 % [26], which, as the authors proposed, makes nitrous and nitric acid close to liquid-phase steam; the authors did not conduct tests under ambient temperature for comparison. Chen et al. [27] showed SO<sub>2</sub> and NO<sub>x</sub> removal by Ca(OH)<sub>2</sub> and concluded that the presence of SO<sub>2</sub> could enhance the efficiency of NO<sub>x</sub> removal. However, their test was also carried out at a high temperature (70 °C) with a Ca(OH)<sub>2</sub> slurry that was pre-treated with water at H<sub>2</sub>O/CaO ratio of 5 [27]. Therefore, the inability of Ca(OH)<sub>2</sub> to sequester NO<sub>x</sub> in this study is likely related to the use of lower temperature and relative humidity (temperature of 23 ± 2 °C and relative humidity of 50 ± 2 %), which are in fact representative of field conditions for much of the world's concrete infrastructure. Further studies are warranted to examine the influence of temperature and relative humidity on the potential for NO<sub>x</sub> interaction with Ca(OH)<sub>2</sub>.

### 3.3. Mono-sulfoaluminate (AFm-SO<sub>4</sub>)

AFm-SO<sub>4</sub> shows significantly lower NO<sub>x</sub> uptake compared to C-S-H but does exhibit some capacity for sequestering NO<sub>x</sub>. Approximately 3 mg kg<sup>-1</sup> of nitrite is measured by wet-chemical extraction while no detectable nitrate is measured (Fig. 2). The XRD pattern for AFm-SO<sub>4</sub> before and after NO<sub>x</sub> exposure has been previously reported in Jin et al. [6] and is reproduced in Fig. 5. Two new peaks at 9.5° and 15.1° 2θ were observed. According to Glasser et al. [29], the newly formed peaks represent the formation of AFm-NO<sub>2</sub>/NO<sub>3</sub>. Thermodynamically, it has been demonstrated that NO<sub>2</sub><sup>-</sup> and NO<sub>3</sub><sup>-</sup> have a binding preference within AFm phases, with a preference of NO<sub>3</sub><sup>-</sup> > NO<sub>2</sub><sup>-</sup> > SO<sub>4</sub><sup>2-</sup> > OH<sup>-</sup> [30]. Therefore, the result provides direct evidence that NO<sub>3</sub><sup>-</sup> and/or NO<sub>2</sub><sup>-</sup> can substitute SO<sub>4</sub><sup>2-</sup> in AFm phase in a solid-gas anion exchange reaction and form crystalline AFm-NO<sub>2</sub>/NO<sub>3</sub>. The lower amount of nitrate detected by wet chemical extraction than nitrite suggest potential preferable binding of nitrate in AFm phase because the anion exchange process of nitrate took precedence over nitrite [30]. Overall, as discussed in Jin et al. [6], this detection provides further insights that aluminate-rich cementitious materials, with their aluminate-bearing phases, could bind NO<sub>x</sub> more permanently through this anion exchange process.

### 3.4. Calcite (CaCO<sub>3</sub>)

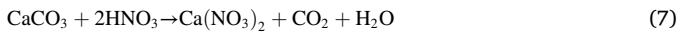
Carbonation is inevitable in cementitious materials, and the most stable carbonation product of both Ca(OH)<sub>2</sub> and C-S-H is calcite [31].



**Fig. 5.** Two new peaks at 2θ of 9.5° and 15.1° were observed in the XRD patterns of AFm-SO<sub>4</sub> phases before (control) and after NO<sub>x</sub> exposure, indicating the formation of AFm-NO<sub>2</sub>/NO<sub>3</sub> phases due to NO<sub>x</sub> uptake [6].

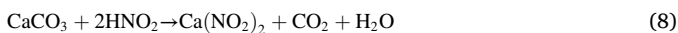


Thus, this study also examined the effects of carbonation on  $\text{NO}_x$  sequestration capability. As shown in Fig. 2, calcite exhibits  $\text{NO}_x$  uptake capacity while portlandite exhibits undetectable  $\text{NO}_x$  uptake. This result indicates that under current environmental conditions ( $23 \pm 2$  °C and relative humidity of  $50 \pm 2$  %) carbonation improves the  $\text{NO}_x$  uptake capability of portlandite. Similar observation of  $\text{NO}_x$  uptake by the mineral calcite was reported by Grassian [9] under a relative humidity of 20 %, where  $\text{NO}_x$  was converted into the gas-phases  $\text{HNO}_3$  which further reacted with calcite to form  $\text{Ca}(\text{NO}_3)_2$ .



Compared to C-S-H, calcite also exhibits a higher  $\text{NO}_x$  uptake capacity (Fig. 2). As discussed in Section 3.1, the converted  $\text{NO}_2^-$  and  $\text{NO}_3^-$  likely adsorb on the surface of C-S-H or dissolve in the pore solution. The higher  $\text{NO}_3^-$  uptake suggests that the chemical reactions between gas-phases  $\text{HNO}_2/\text{HNO}_3$  and  $\text{CaCO}_3$  are more effective in  $\text{NO}_x$  uptake than the binding mechanism of C-S-H.

According to Fig. 2, the total  $\text{NO}_x$  uptake of calcite comprises nitrite of approximately  $14 \text{ mg kg}^{-1}$  and nitrate of  $540 \text{ mg kg}^{-1}$ , with  $\text{NO}_2^-$ -to- $\text{NO}_3^-$  ratio of 1:38. Therefore, it is expected that a small amount of  $\text{NO}_x$  has converted to gas-phases  $\text{HNO}_2$  and reacted with calcite in a similar manner as gas-phases  $\text{HNO}_3$  [9], which is described in Eq. (8). The significantly higher concentrations of  $\text{NO}_3^-$  compared to  $\text{NO}_2^-$  suggests that under the current environmental conditions the heterogeneous surface-related reactions of calcite seem to favor the formation of  $\text{Ca}(\text{NO}_3)_2$ .



XRD was also performed to examine the formation of  $\text{Ca}(\text{NO}_2)_2$  and  $\text{Ca}(\text{NO}_3)_2$ . Interestingly, no noticeable new peaks were detected by XRD (Fig. 6). This is possibly due to the highly hygroscopic nature of the formed  $\text{Ca}(\text{NO}_2)_2$  and  $\text{Ca}(\text{NO}_3)_2$ . Instead of using XRD, Grassian [9] used Fourier-transform infrared spectroscopy (FTIR) and transmission electron microscopy (TEM) to confirm the formation of  $\text{Ca}(\text{NO}_3)_2$ . In addition, they also discovered an increased formation of a water layer on the surface of reacted calcite, which further promotes  $\text{NO}_x$  adsorption and the formation of  $\text{Ca}(\text{NO}_3)_2$ .

### 3.5. Mono-carboaluminate (AFm- $\text{CO}_3$ )

The effect of carbonation of AFm on  $\text{NO}_x$  uptake was examined using AFm- $\text{CO}_3$  as the mono-carboaluminate is the most stable carbonated AFm phase in concrete [16]. Compared to AFm- $\text{SO}_4$ , higher amounts of  $\text{NO}_2^-$  and  $\text{NO}_3^-$  were detected through wet chemical extraction (Fig. 2), and no new phases were detected by XRD (Fig. 7). These results suggest that the  $\text{NO}_x$  binding mechanism might be surface adsorption, which

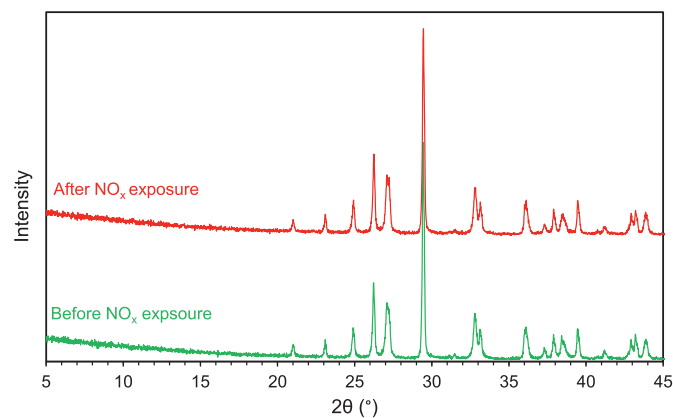


Fig. 6. No new peaks were observed in the XRD patterns of calcite before (control) and after  $\text{NO}_x$  exposure, suggesting that the formed  $\text{Ca}(\text{NO}_2)_2$  and/or  $\text{Ca}(\text{NO}_3)_2$  could be highly hygroscopic and undetectable by XRD.

could be detected and measured by the wet chemical extraction used in this study. Since both AFm phases have similar morphologies and surface features [32,33], the results further indicate that the anion exchange process, which was observed in AFm- $\text{SO}_4$  phase, may not occur in the carbonated AFm phase.

## 4. Discussion

### 4.1. Transiency and permanency of $\text{NO}_x$ binding

Since C-S-H and  $\text{Ca}(\text{OH})_2$  are the main phases in OPC-based cementitious materials, the transient binding mechanisms of these two phases confirm our previous observation that  $\text{NO}_x$  binding in OPC-based cementitious materials is largely transient and susceptible to water-based wet chemical extraction [5]. Additionally, the fact that  $\text{NO}_2^-$  and  $\text{NO}_3^-$  ions in both C-S-H or calcium nitrite/nitrate are susceptible to water-based chemical extraction suggests high mobility of the produced nitrate/nitrite, which also helps partially explain the previous observations that the  $\text{NO}_x$  binding capacity could be recovered after the samples were subjected to water, such as during rainfall [4,7]. However, the transient  $\text{NO}_x$  binding could be problematic as the nitrites and nitrates could be released back to groundwater, aquatic and forest systems, or into agricultural systems [34]. For example, certain amounts of  $\text{NO}_2$ , which is produced in the photocatalytic process, could be released back to the environment [35,36]. In addition, the transient  $\text{NO}_x$  binding could potentially be harmful to the photocatalytic  $\text{TiO}_2$ -modified cementitious materials. For example, the nitrous and nitric acids that are formed through photocatalytic reactions could cause decomposition of the C-S-H and  $\text{Ca}(\text{OH})_2$  phases and compromise the surface integrity and mechanical properties of the material [37].

Based on Section 3.3, the  $\text{NO}_x$  binding in aluminate rich phases such as AFm appears to be more permanent, providing a potential pathway to overcome these concerns and enhance the sustainability of  $\text{NO}_x$  sequestration. Therefore, to improve the potential for permanent  $\text{NO}_x$  binding, calcium aluminate cement (CAC) with higher aluminate content (compared to OPC) could be advantageous for this application. Our previously study [6] has demonstrated that  $\text{NO}_x$  uptake through photocatalytic reactions in CAC-based cementitious materials can only be partially recovered by water-based wet chemical extraction. The results further validate the anion exchange process in  $\text{NO}_x$  binding within AFm- $\text{SO}_3$  phase that is observed in this study.

### 4.2. Effect of carbonation on $\text{NO}_x$ binding

This study has shown that the carbonation of cementitious material

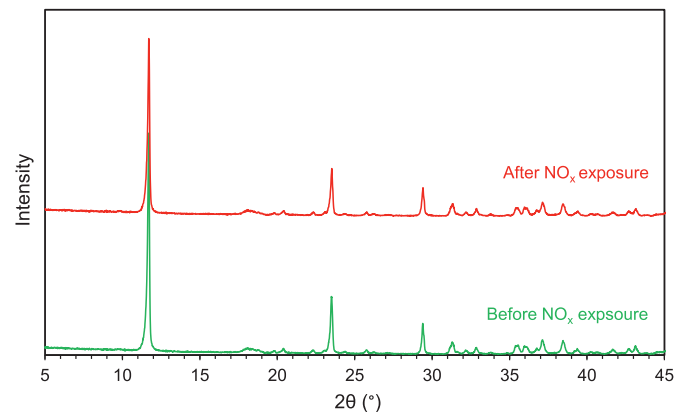


Fig. 7. No new peaks were observed in the XRD patterns of AFm- $\text{CO}_3$  phases before (control) and after  $\text{NO}_x$  exposure, suggesting that the anion exchange process, which has been observed in AFm- $\text{SO}_4$  phase (Fig. 6), may not occur in AFm- $\text{CO}_3$ .

could positively impact  $\text{NO}_x$  sequestration. According to the Fig. 2, the uptake capacity of  $\text{CaCO}_3$  phases is three times that of C-S-H, suggesting that carbonation could be a potential pathway to increase  $\text{NO}_x$  binding capacities in cementitious materials. Kaja et al. [15] have observed a similar enhancement of  $\text{NO}_x$  degradation in a carbonated portlandite-rich mortar and concluded that the carbonation of calcium-bearing phases increases the formation of capillary pores resulting in enhanced  $\text{NO}_x$  degradation. Based on the results from Section 3.4, this phenomenon could be further explained by including the additional heterogeneous  $\text{NO}_x$  binding pathway of  $\text{CaCO}_3$ , which increases the potential chemical sink for  $\text{NO}_x$ , especially when the reactions are not only on the surface of the  $\text{CaCO}_3$  particles but also occur in bulk mixtures [9]. Moreover, since carbonation usually initiates from the concrete surfaces, this favors  $\text{NO}_x$  uptake as the surfaces are also directly exposed to  $\text{NO}_x$ . The released  $\text{CO}_2$  from the reactions (Eqs. (7) and (8)) could carbonate other uncarbonated  $\text{Ca(OH)}_2$  phases, resulting in further enhanced  $\text{NO}_x$  binding capacity. Therefore, the carbonation of cement-based materials could potentially increase the material's  $\text{NO}_x$  sequestration capacity even with low surface area and lack of interlayer water and pore solution-containing pores. However, as the mass of carbonated C-S-H,  $\text{Ca(OH)}_2$ , and  $\text{CaCO}_3$  are not the same in cementitious materials, more  $\text{CO}_2$  uptake is possible by the carbonation of  $\text{Ca(OH)}_2$  than C-S-H and composition can be adjusted to enhance binding. Further studies are needed to quantify and compare the  $\text{NO}_x$  uptake potentials between uncarbonated and carbonated phases based on their mass fractions and degree of carbonation. Additionally, the effect of re-released  $\text{CO}_2$  on the sustainability concerns should be examined in the future study.

The carbonation of AFm phases, as shown in Section 3.5, could potentially inhibit the anion exchange process and result in a transient  $\text{NO}_x$  binding. According to Balonis [30,38],  $\text{NO}_2^-$  and  $\text{NO}_3^-$  should have a greater thermodynamic occupation preference than  $\text{CO}_3^{2-}$ . However, this conclusion was based on the interaction of ionic solution and solid phases [30,38]. As demonstrated in this study, without an abundant presence of water, the difference in the thermodynamic occupation preference between  $\text{NO}_2^-$  and  $\text{NO}_3^-$  ions and  $\text{CO}_3^{2-}$  ions may not be significant, thus preventing the anion exchange. Therefore, the water molecules that are associated with carbonated AFm phases are critical for the anion exchange process to occur and thereby maintain the benefits of AFm- $\text{SO}_4$  phases.

## 5. Conclusion and future perspectives

In this study, five cementitious phases, calcium silicate hydrate, portlandite, mono-sulfoaluminate, calcite, and mono-carboaluminate were tested for their  $\text{NO}_x$  uptake, toward understanding their binding capacity and mechanisms. A combined method of wet chemical extraction, UV-vis spectrophotometry, and ion chromatography was used to quantify  $\text{NO}_x$  uptake and to delineate between nitrite and nitrate uptake. Together with XRD analysis, the  $\text{NO}_x$  sequestration mechanisms were examined. The effect of carbonation on  $\text{NO}_x$  binding was examined by comparing uncarbonated phases with carbonated ones. With this information on  $\text{NO}_x$  capacities and binding mechanisms for each cementitious phase, this study could provide guidelines for engineers and scientists to properly design a cement-based material that has a desired chemical composition and microstructural features for enhanced  $\text{NO}_x$  sequestration. Some key insights are summarized as follows.

1. Among uncarbonated phases, C-S-H shows the highest  $\text{NO}_x$  uptake capacity. The  $\text{NO}_2^-$  and  $\text{NO}_3^-$  produced as a result of  $\text{NO}_x$  conversion either adsorb on the surface of the C-S-H phase or dissolve in the pore solution. The  $\text{NO}_x$  conversion may not occur in  $\text{Ca(OH)}_2$  phases due to the environmental conditions used in this study (relative low temperature and relative humidity). The  $\text{NO}_2^-$  and  $\text{NO}_3^-$  ions interact with the AFm- $\text{SO}_4$  phases by substituting for sulfate ions to form AFm- $\text{NO}_2/\text{NO}_3$  phases, which could be detected by XRD.

2. For carbonated phases,  $\text{CaCO}_3$  exhibits an improved  $\text{NO}_x$  sequestration capacity compared to uncarbonated phases, with a  $\text{NO}_x$  uptake capacity *three times* higher than that of C-S-H. This higher capacity could be attributed to the reactions between the produced nitrite and nitrate and the  $\text{CaCO}_3$  and can occur both on the surface of the  $\text{CaCO}_3$  particles and in the bulk mixtures. However, the formed  $\text{Ca(NO}_2)_2$  and  $\text{Ca(NO}_3)_2$  could not be detected by XRD, possibly due to the poor crystallinity of the formed products. The carbonation of AFm- $\text{SO}_4$  phases could potentially inhibit the anion exchange process that was observed in uncarbonated AFm- $\text{SO}_4$  phases; and  $\text{NO}_x$  likely adsorb on the surface of the solids of AFm- $\text{CO}_3$ .

Based on the results and conclusion, the following future studies are recommended. Additional studies need to be performed on the C-S-H with different Ca/Si ratio. This study has revealed that both temperature and water play an important role in  $\text{NO}_x$  sequestration capacities and pathways in hydrated cementitious phases. In concrete infrastructure, a major source of water is the relative humidity in the environment. Therefore, additional experiments are needed to confirm the impact of temperature and relative humidity on  $\text{NO}_x$  sequestration by cementitious phases. As aluminate-bearing phases could potentially provide a more permanent  $\text{NO}_x$  binding, future research could consider including other common aluminate phases in cementitious materials such as C-A-S-H,  $\text{AH}_3$ ,  $\text{C}_3\text{AH}_6$ , and  $\text{C}_2\text{AH}_8$ . As amorphous phases (e.g., amorphous  $\text{CaCO}_3$  and amorphous silica gel) also exist in concrete, these phases should also be studied in the future to understand their binding mechanisms relative to the crystalline phases examined here. More importantly, it remains unclear how these binding mechanisms occur in hydrated cementitious phases: whether they occur simultaneously or sequentially. In addition, it is also important correlate the  $\text{NO}_x$  uptake potential with the surface area and pore structure. Since nitrite and nitrate can be used at the steel interface to improve the corrosion resistance of steel-reinforced concrete, a future study could be carried out to understand and quantify the potential resistance against chloride-induced corrosion by tailoring cementitious materials with different C-S-H,  $\text{CaCO}_3$ , and AFm- $\text{SO}_4$  content.

## CRediT authorship contribution statement

**Qingxu Jin:** Conceptualization, Investigation, Methodology, Validation, Formal analysis, Data Curation, Visualization, Project administration, Writing - Original Draft, Writing - Review & Editing.

**Samuel N. Lucas:** Investigation, Data Curation, Writing - Review & Editing.

**Yuanzhi Tang:** Methodology, Resources, Writing - Review & Editing.

**Kimberly E. Kurtis:** Conceptualization, Resources, Project administration, Writing - Review & Editing, Supervision, Funding acquisition.

## Declaration of competing interest

None.

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